

Digital Predistortion of Power Amplifier Non-Linearities for Full-Duplex Transceivers

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Predistortion of Power Amplifier Non-Linearities

Power amplifiers can introduce significant non-linear components into the transmitted signal

- For wideband signals, **memory effects** aggravate the problem

Digital predistortion compensates for non-linear compression and memory effects by appropriately pre-processing the **baseband signal**

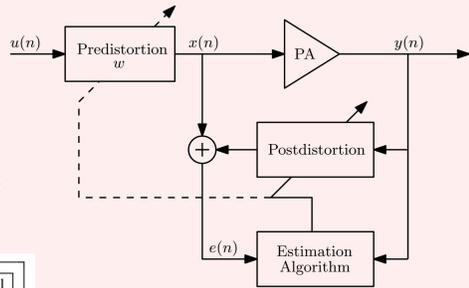
Predistortion requires a model of the power amplifier to find the **inverse**:

- Memory polynomial:
$$y(n) = \sum_{k=0}^{K-1} \sum_{m=0}^{M-1} a_{km} x(n-m) |x(n-m)|^k$$

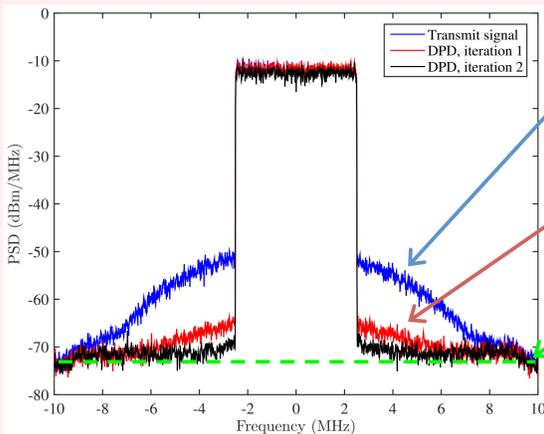
Coefficients Basis function

Determining the Coefficients:

- Find predistortion coeffs by using PA output y to estimate the PA input x via least-squares
- After convergence: copy coeffs to predistortion stage and run open-loop



Experimental Verification:



No predistortion: strong out-of-band emissions 40 dB down from peak power

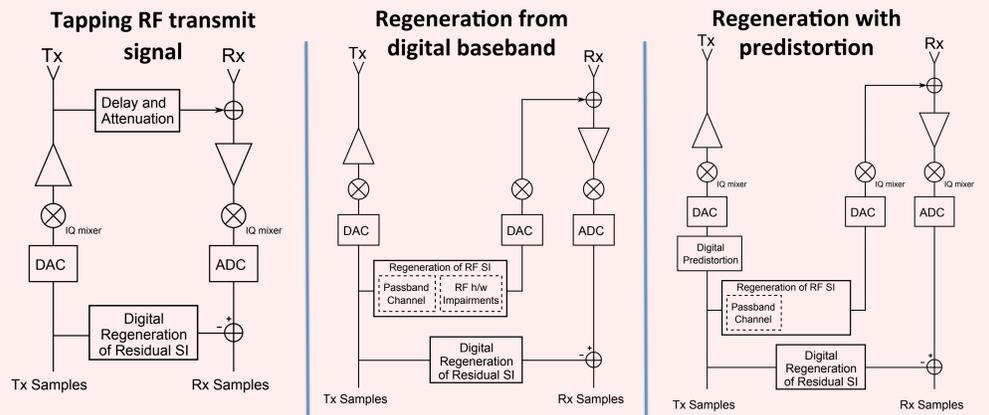
Predistortion with $K = 8$ and $M = 8$: rejection of out-of-band emissions by 20 dB to slightly above noise-floor

Noise-Floor: set by the approx 66 dB dynamic range of the receiver ADC
2.4 GHz carrier, 20 dBm, 5 MHz, 512-tone OFDM

Application to Full-Duplex Transceivers

Full-duplex transceivers based on **digital regeneration**: more sensitive to PA non-linearities (and other impairments) than analog cancellation architectures

Predistortion reduces non-linearities in transmit signal: **reduces required complexity of cancellation at the receiver**



- Inherently captures all TX non-idealities
- Requires reconfigurable analog hardware: **does not scale well for MIMO**

- All signal processing done digitally: **scales well for MIMO**
- Requires precise modelling and reconstruction of TX non-idealities

- Linearizing the TX signal means less non-linear cancellation is required
- Avoid modelling the PA memory in digital cancellation

Memory polynomial predistortion **only** accounts for the power amplifier: mixer IQ-imbalance and DAC baseband non-linearities are also significant

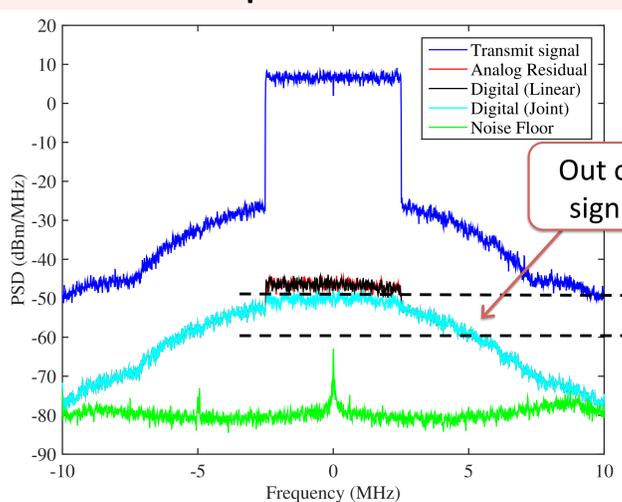
- New predistortion IQ and PA basis** that includes mixer and DAC effects:

$$y(n) = \sum_{f=0}^F \sum_{g=0}^G \sum_{m=0}^M a_{fgm} \Re\{x'(n-m)\}^{\frac{f}{2}} \Im\{x'(n-m)\}^{\frac{g}{2}}$$

a_{fgm} : coefficients
 M : memory depth
 F : max. exponent of Real Part
 G : max. exponent of Imaginary Part

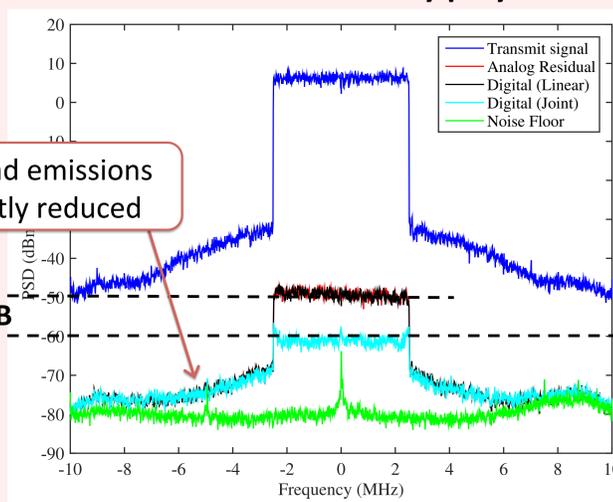
Experimental Measurements of Self-Interference Suppression with Predistortion

No predistortion



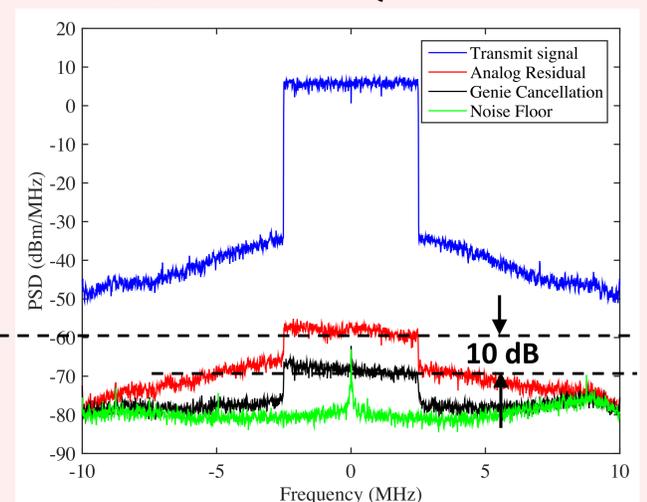
- Digital cancellation stage unable to reduce self-interference more than analog stage
- Self-interference approx 30 dB above the noise

Predistortion with memory polynomial



PA predistortion allows digital cancellation stage to reduce self-interference further by 12 dB

Predistortion with IQ and PA basis



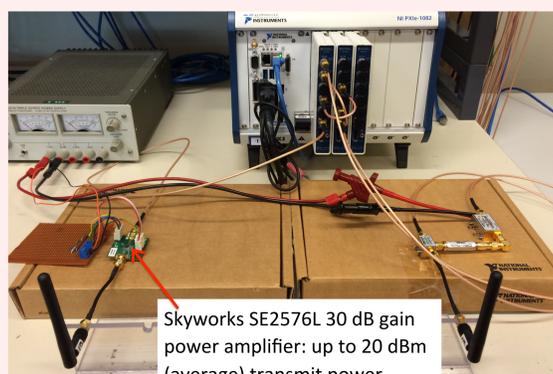
- Analog cancellation stage **alone** reduces self-interference to within 20 dB of the noise-floor (on the same level as digital with PA linearization)

Hardware Testbed

- NI FlexRIO PXIe-1082 with two NI-5791 RF modules
- Baseband signal processing performed in Matlab

Two stage self-interference suppression:

- RF cancellation signal generated from digital baseband (by sounding self-interference channel)
- Digital cancellation applied to the residual self-interference (joint model includes IQ-imbalance)



Skyworks SE2576L 30 dB gain power amplifier: up to 20 dBm (average) transmit power

What is in the residual?

- A "feasible" genie removes all deterministic signal components by averaging over 10 frames

The genie predicts an additional 10 dB analog or digital suppression is possible

- The remaining self-interference (10 dB above the noise-floor) comes from random components, e.g., phase-noise or timing jitter