

Modelling Inter-Floor Radio-Wave Propagation in Office Buildings

A. C. M. Austin*, M. J. Neve and G. B. Rowe

Department of Electrical and Computer Engineering
The University of Auckland, Auckland, New Zealand

Motivations

- Performance and capacity of wireless systems limited by **interference**
- Interfering power levels are heavily influenced by the environment
- Propagation in indoor environments is not well understood
- Coverage/interference prediction tools are required



How does the energy travel between the floors?

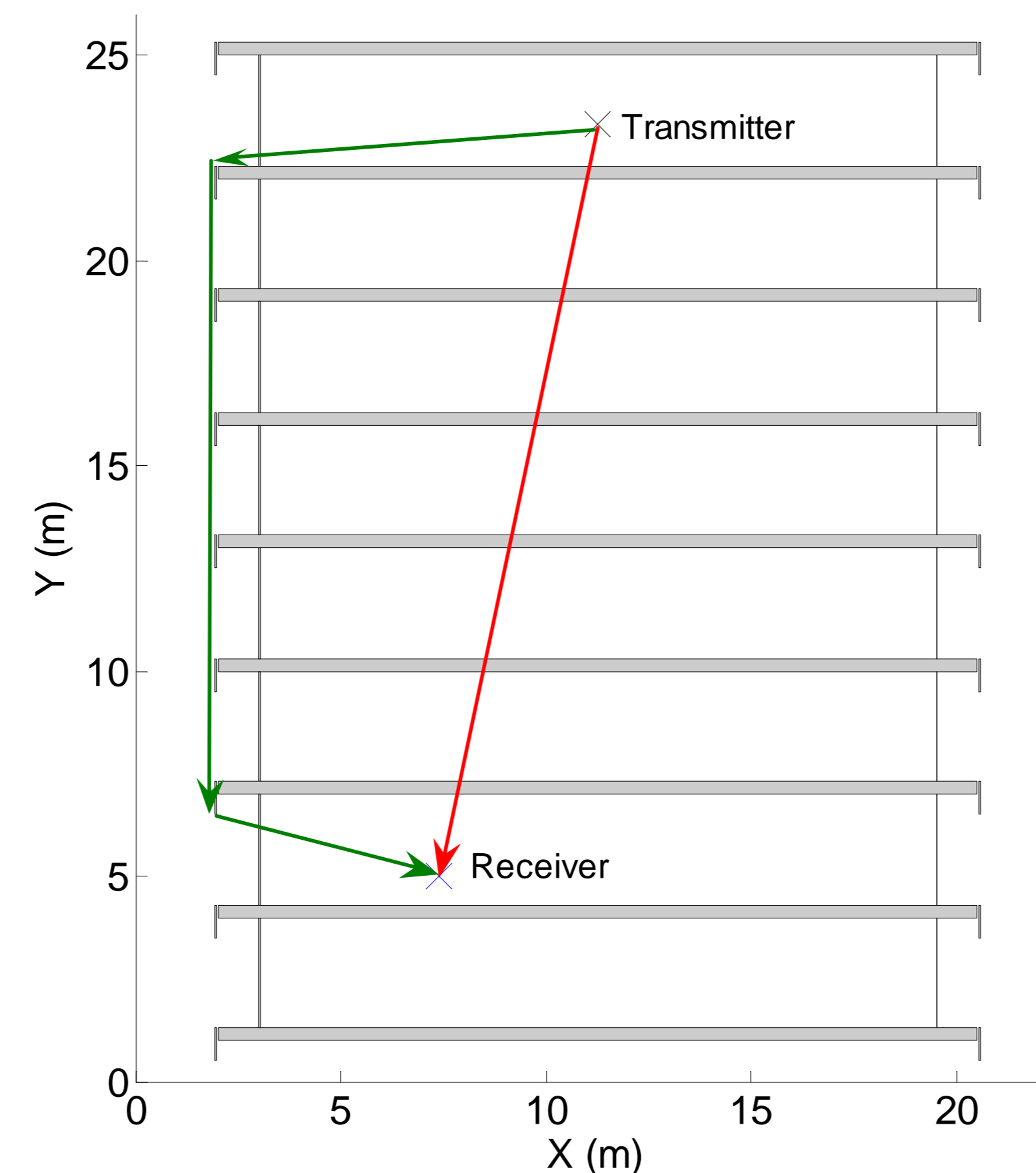
and

How can we model this behaviour?

Inter-Floor Propagation

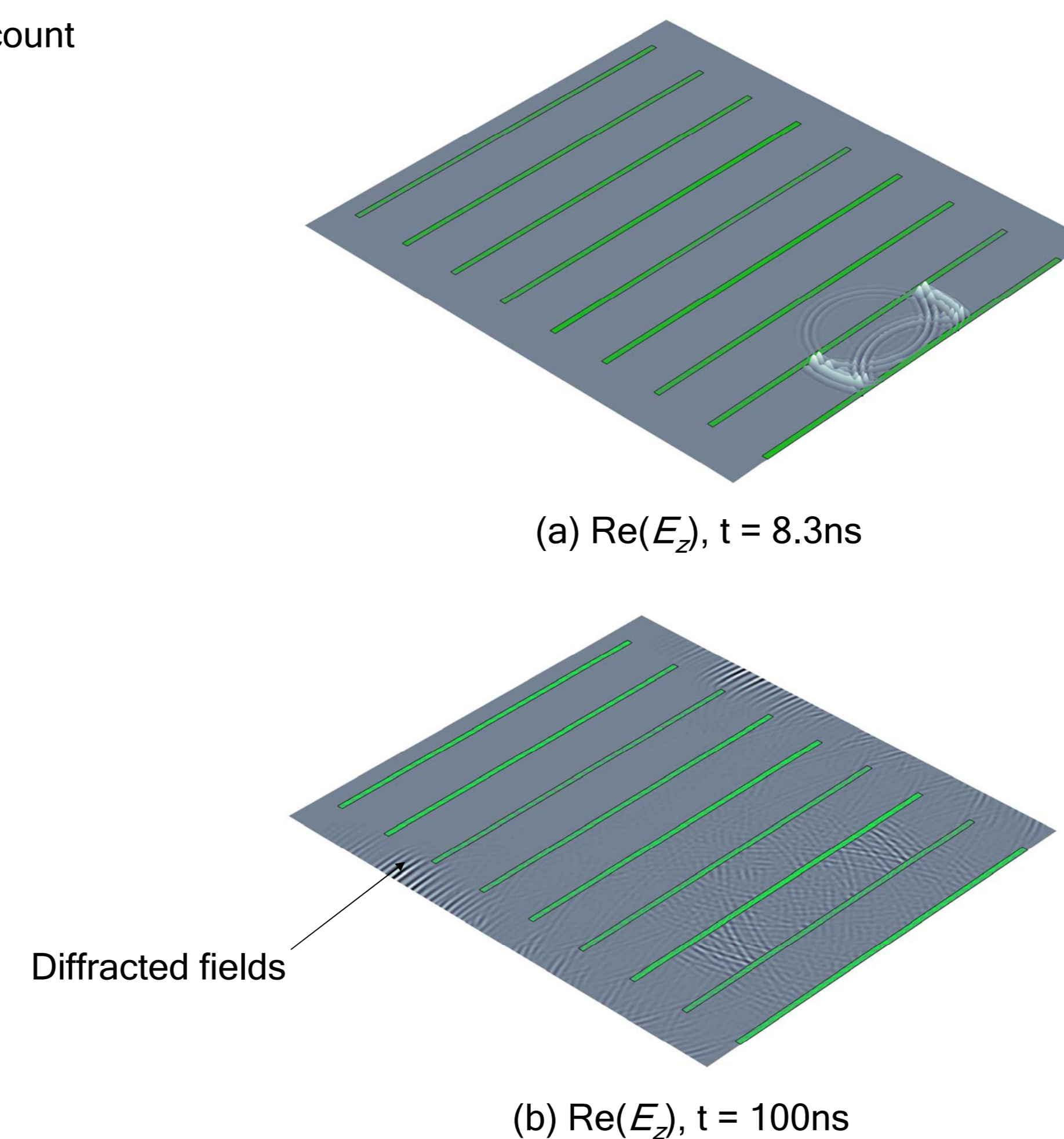
- Results show two propagation paths: **Direct Penetration** and **Floor-Edge Diffraction**
- A simple mechanistic model takes both components into account

What level of accuracy will this model provide?



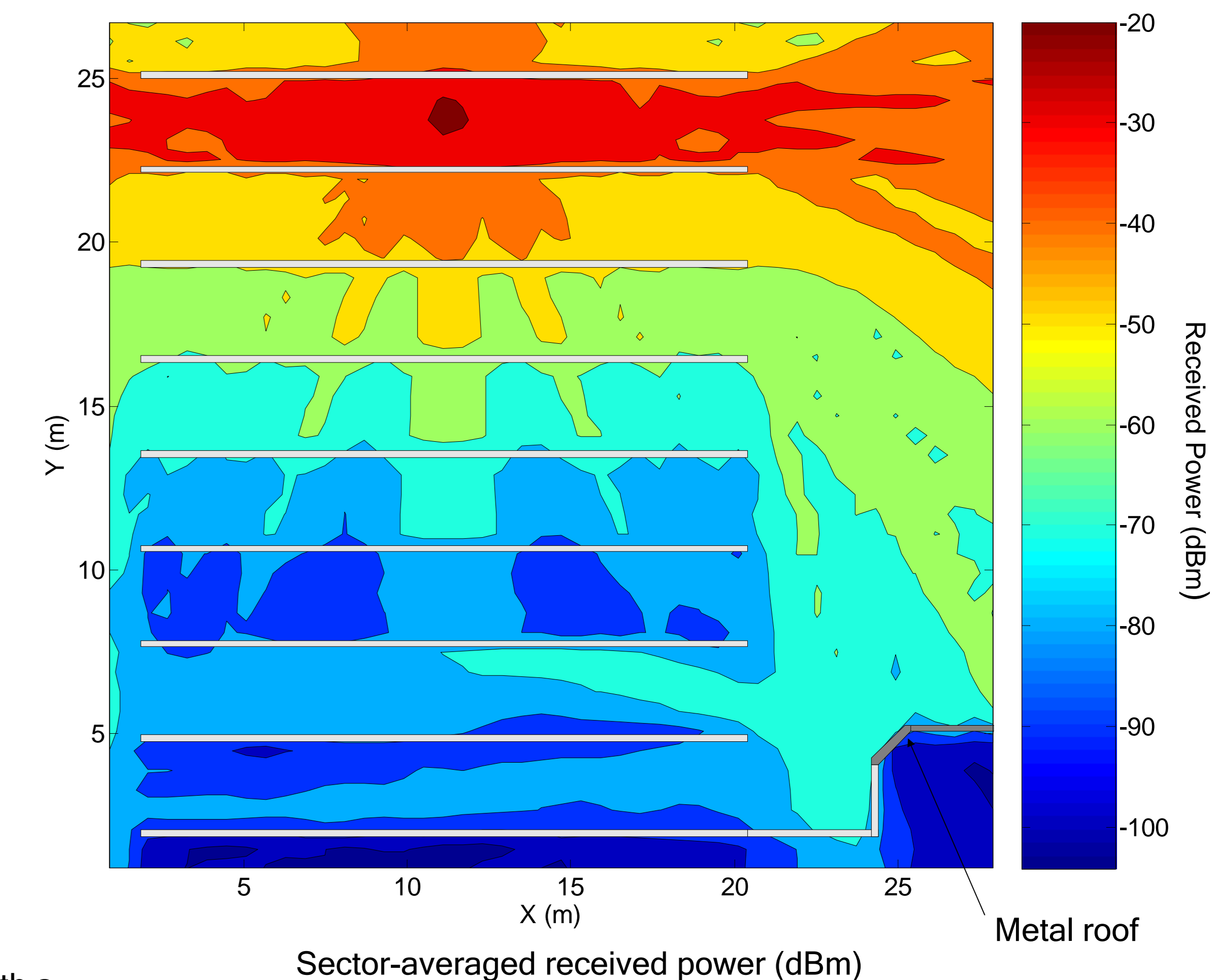
Visualisation

- The lattice is excited with a modulated Gaussian pulse, and the wave fronts observed



Effects of Nearby Buildings

- Nearby buildings can reflect significant levels of power back onto lower floors
- The increase is up to **22 dB** over the case where no nearby building is present



Features of a Desirable Solution

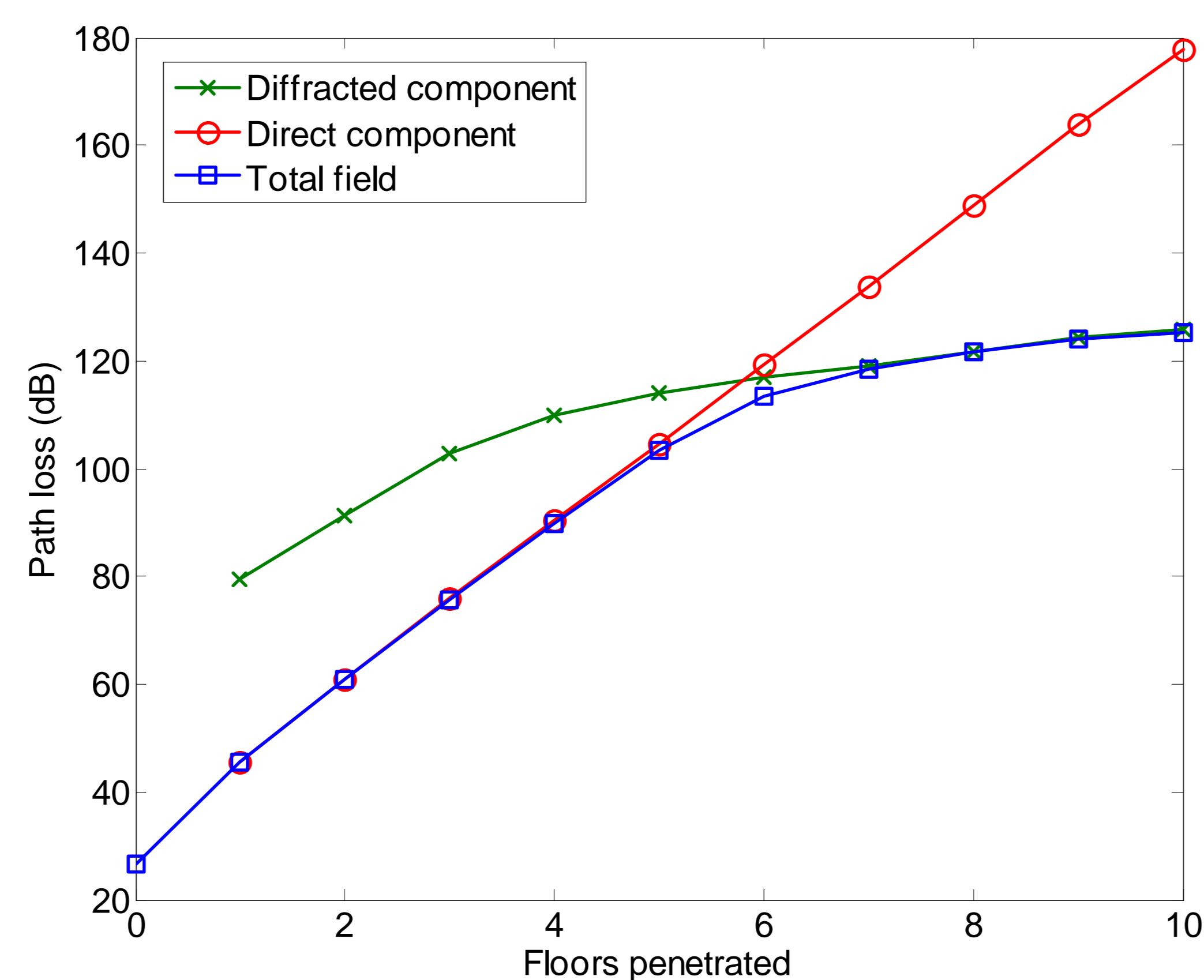
- Deterministic **Electromagnetic** basis
- Explains experimental results
- Transportable (i.e. can be used in other buildings)
- Provide a basis on which to build approximate, yet reliable/efficient models for system design purposes

Identifying the Mechanisms

- A 2D implementation of the **Finite-Difference Time-Domain** algorithm is used to determine the mechanisms governing inter-floor propagation
- A vertical slice through the problem is analysed at 1.0GHz for TM polarization
- The concrete floors are modelled as dielectric slabs:
 - $\epsilon_r = 6.0$
 - $\sigma = 50 \text{ mS/m}$
 - Floor thickness: 0.30 m
 - Floor-ceiling separation: 2.70 m
- External building features, e.g. windows and hanging panels have also been modelled

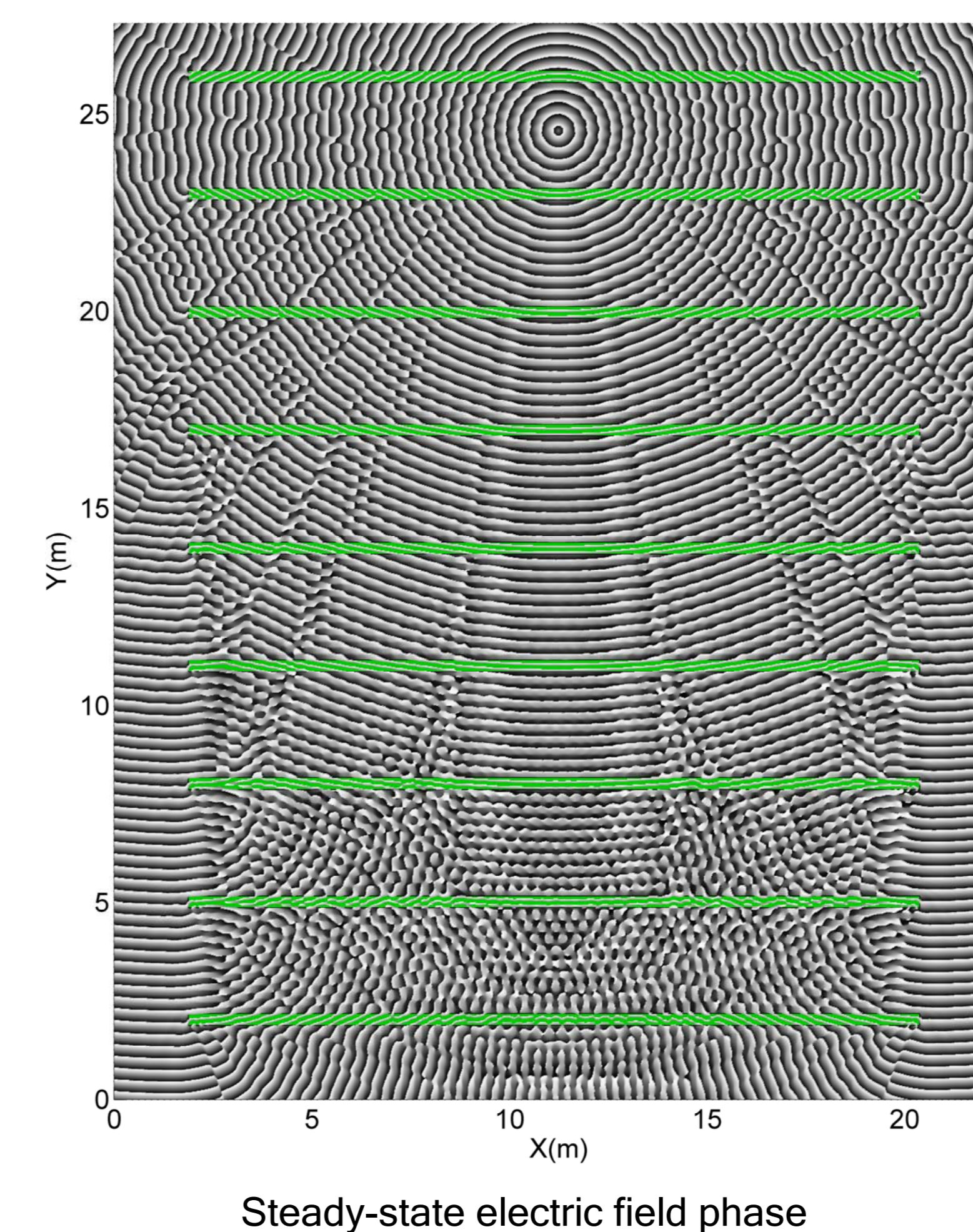
Results – 1.0 GHz TM_z Polarization

- The received power is averaged across small sectors to remove multipath fading



- Diffraction dominates the total power after 5-6 floor penetrations
- This finding agrees well with previously unexplained experimental results

- The steady-state electric field phase at 1.0GHz is extracted with a Fourier transform



- The curvature of the steady-state electric field phase remains centred on the source point for < 6 floor penetrations
- Diffraction at the floor edges is clearly visible after 5 floor penetrations

Mechanistic Model

FDTD results suggest:

- The direct component can be modelled as free space with an appropriate (linear) **floor attenuation factor**

$$P_{\text{direct}} = P_{\text{free space}} + N \cdot \text{FAF} \quad (\text{dB})$$

- The diffracted component is best modelled by multiple diffraction at the floor edges
- Initial results suggest an additional distance dependency term of:

$$20 \log_{10} \left(\frac{1}{N+1} \right) \quad (\text{dB})$$

Conclusions

- Direct penetration through the floors dominates the total received power for less than five floor penetrations
- The dominant **mechanism changes** to diffraction after six floor penetrations
- Results suggest a simple two-component model will be appropriate to predict area coverage
- Nearby buildings must also be considered, as preliminary results show the received power can be increased by 22 dB